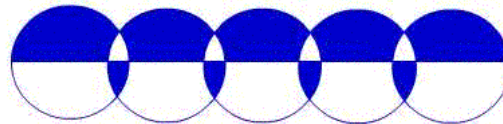




Membrane Technologies and Supercritical Fluids: Chemical Engineering for coupled processes

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- Presentation of the Membrane Processes Team (USACH)
- SCF and Membrane Technology: State of the art
- Separation of mixtures containing supercritical solvents through microporous membranes
- Coupling SCF and no conventional membrane processes: modeling and simulation of the extraction by membrane contactors using supercritical solvents



Laboratory of Membrane Processes

Dr. Aldo Saavedra, Dr. Julio Romero, Dr. Valeri Bubnovich

14 under graduate y graduate students

Participation in 10 Research Projects (FONDECYT, FONDEF, USACH and UNESCO) from 1995

Research Subjects

- ✓ Applications of MF, UF, NF and RO to food industry and wastewater treatment
- ✓ ED and polyelectrolyte enhanced ultrafiltration (PEUF) for treatment of drinking water
- ✓ Membrane contactor operations (OD, MD, VMD and liquid-liquid extraction)
- ✓ Processes coupling SCF and Membrane Technology (separation by microporous membranes and porocritical extraction)

International cooperation

European Institute of Membranes (CNRS, Montpellier, France), **University of San Luis** (Argentina), **Joint Research Team “Supercritical Fluids and Porous Media”** (CEA/CNRS/UM2/ENSCM)

From 1992: Several membrane applications connected to SC CO₂

Improvement of membrane preparations in term of chemical resistance



Fractionation of SC CO₂/EtOH and SC CO₂/isooctane using asymmetric Kapton® membrane
(*Semenova and Ohya, 1992*)

Fractionation of water/EtOH mixtures in presence of SC CO₂ using a RO membrane
(*Hsu and Tan, 1993*)

When SC CO₂ is used as a solvent for extraction, it is interesting to recover CO₂, without performing a pressure drop



A membrane process is proposed within the SCF cycle reducing drastically the energy losses.

80-90% of low volatile compounds (LVC) discharged from SC CO₂ using a NF membrane
(*Birtigh, 1995; Sartorelli and Brunner, 2000*)

STATE OF THE ART



Nanofiltration coupled to SFE (*Sarrade, 1994*)

NF and SFE are intended to act on the same chemical species (i.e. low molecular weight compounds up to 1500 Dalton)

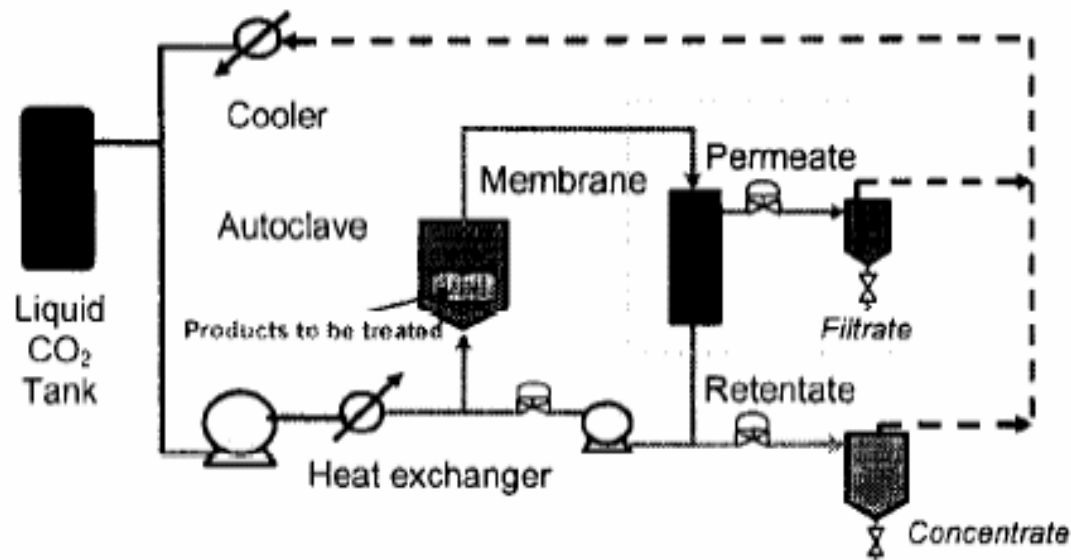
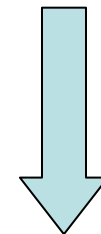


Fig. 1. Nanofiltration plus supercritical fluid extraction process. Flow rate: $0.5\text{--}3\text{ m}^3\cdot\text{h}^{-1}$; $T_{\text{max}} = 423\text{ K}$; $P_{\text{max}} = 35\text{ MPa}$.

Hybrid membranes:
Nafion® layer supported
on a TiO_2 with a mean pore
diameter of about 10 nm)



Mass transfer
mechanism proposed:

CONVECTION ?



Nanofiltration coupled to SFE (*Sarrade, 1994*)

ADVANTAGES

- ✓ High permeate flux (low viscosity of SC CO₂, ten times lower than for water)
- ✓ Good control of the whole extraction/separation process. In the conventional SFE the choice of optimal extraction conditions is often blocked by a preoccupation with a good final fractionating of extracts
- ✓ Two functions (extraction and separation) may be optimised separately

STUDIED SYSTEMS

- Separation of model solutions constituted of small PEGs-SC CO₂
- Extraction/separation of EPA and DHA from fish oils
- Extraction/separation of β -carotene (Provitamin A) and yellow-orange colorants of agro-food industries

SCF assisted ultrafiltration (*Rodriguez et al., 2002*)

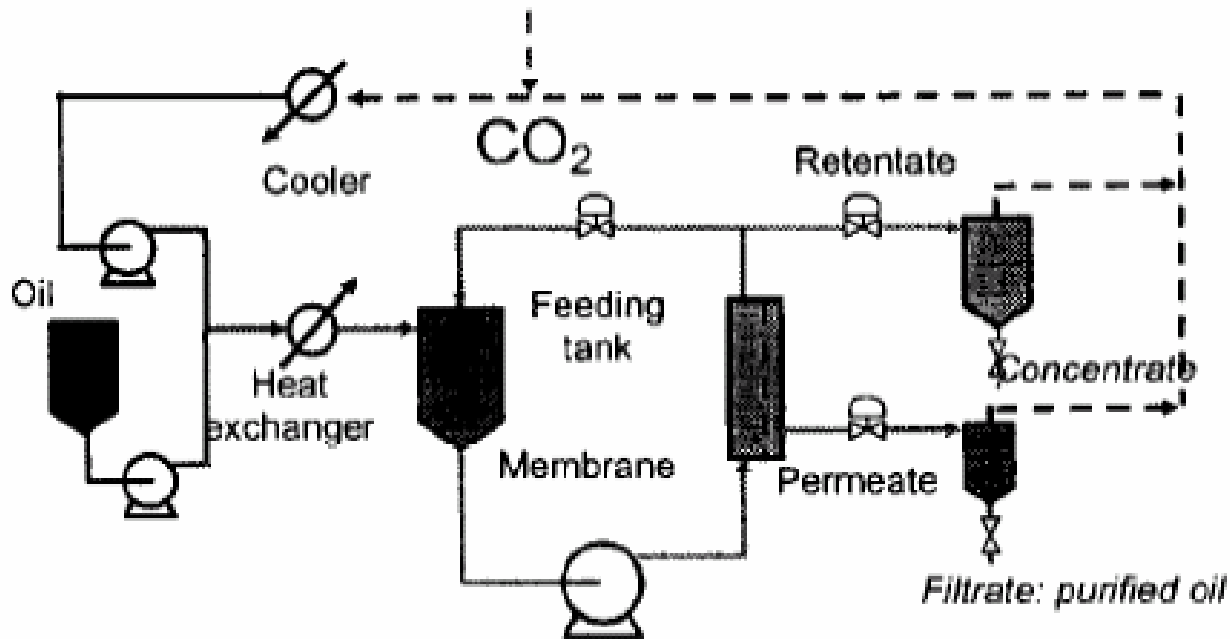


Fig. 2. Pilot-plant for SCF assisted ultrafiltration. Flow rate: $0.5\text{--}3 \text{ m}^3\cdot\text{h}^{-1}$; $T_{\text{max}} = 423 \text{ K}$; $P_{\text{max}} = 35 \text{ MPa}$.



SCF assisted ultrafiltration (*Rodriguez et al., 2002*)

UF of highly viscous liquids (particular oils) is an uneasy and expensive operation (up to 350°C, adding chemicals, improved equipment security)

Low permeate flux and high energy consumption

Cross-flow UF: profiting the properties of SC CO₂ (20 MPa and 150°C)

- *low viscosity*
- *low surface tension*
- *“tunable” solvent power*

PEGs solutions + SC CO₂: viscosity reduced 6 times
Used motor oil + SC CO₂: viscosity reduced 9 times

UF of SC CO₂-used oils

Flow increasing higher than 300%; $P_{opt} = 15$ MPa
Inorganic membrane: ZrO₂ (MWCO = 50-300 kD)

Excellent rejection of metals
(Fe, Zn, Cu): 96% and 99%
depending on species for a
mass concentration factor of
about 27

SCF assisted ultrafiltration (*Rodriguez et al., 2002*)

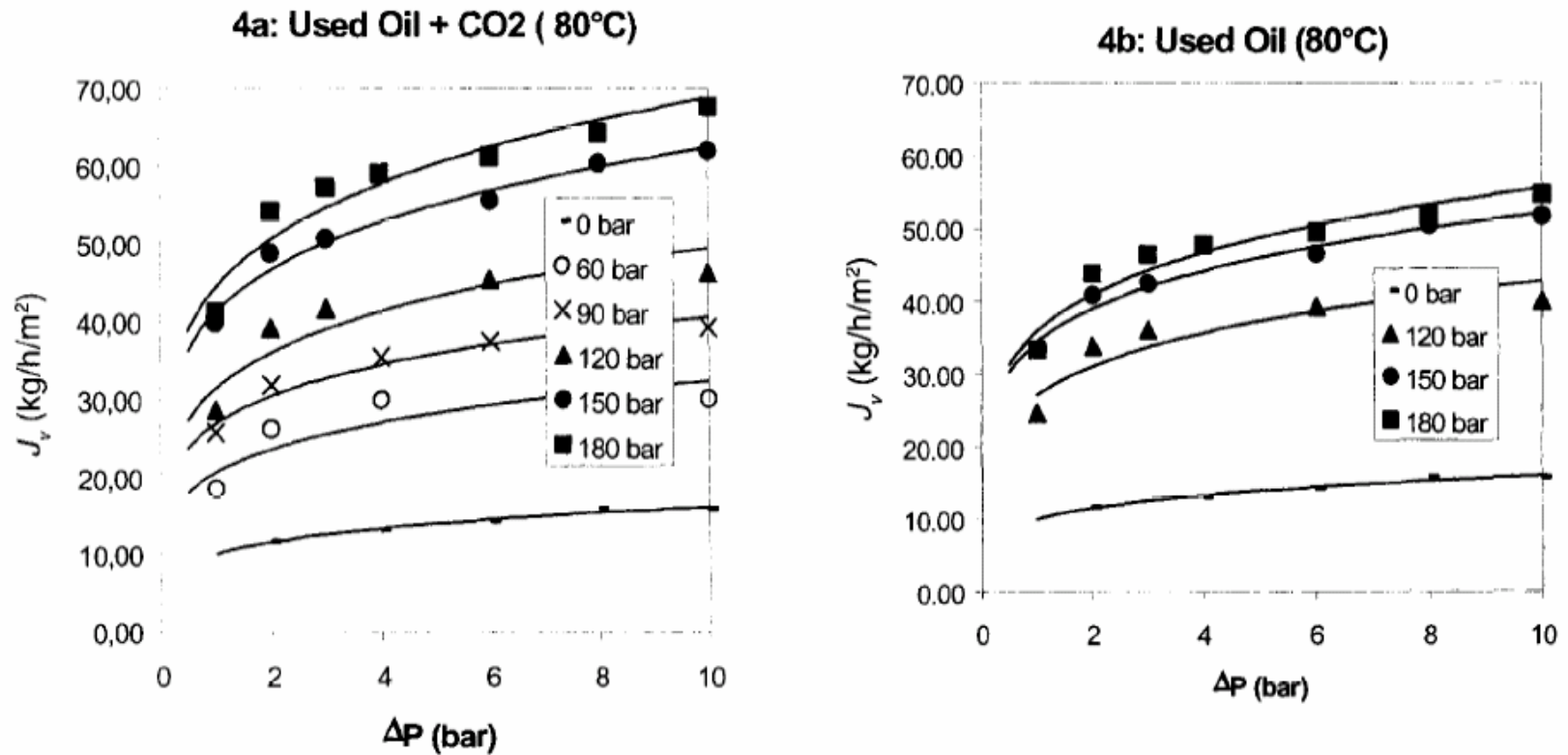
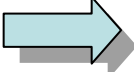


Fig. 4. Influence of transmembrane and CO₂ pressures on oil permeate flux (a): J_v = mixture flux; (b): J_v = net flux in oil).



 **Subject 1:** Permeability and selectivity determination of SCF through microporous membranes (Project FONDECYT 1040240)

Subject 2: Modeling of the extraction by membrane contactors using supercritical solvents: simulations of porocritical extraction



Many questions and few answers:

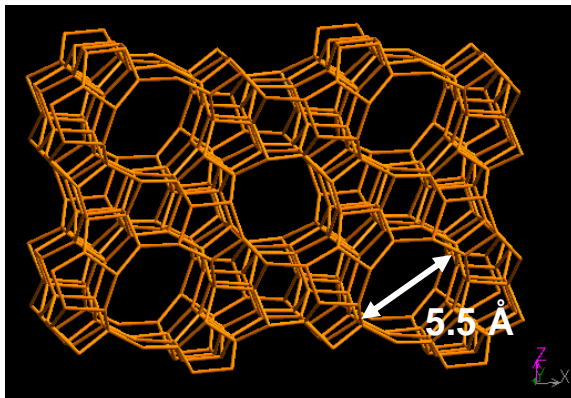
How SCF flow through a microporous membrane?

What is the selectivity mechanism within micropores ($d_p < 2 \text{ nm}$)?

How is the permeation behavior of SCF compared to gas and liquid phases?

CHOSEN SYSTEM:

Permeation of SC CO_2 through a supported MFI zeolite membrane



Thin layer (10-50 μm) of MFI zeolite ($d_p = 5.5 \text{ \AA}$)
deposited on a macroporous $\alpha\text{-Al}_2\text{O}_3$ support



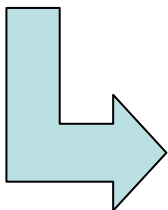
Previous works / **Technical limitations**

Sarrade, 1994: Permeability and selectivity values for PEG-SC CO₂ mixtures using Nafion-TiO₂ membranes / **Proposed mechanism: convection? (presence of defaults?)**

Romero et al., 2001: Permeability values of SC CO₂ and SC N₂O through zeolites membranes / **Variability in the permeance measurements with a continuous flow apparatus ($G_{\text{CO}_2} = 1.8 \cdot 10^{-7} \text{ mol m}^{-2} \text{ s}^{-1} \text{ Pa}^{-1}$), adsorption effect is observed**

Kulcke, 2002: Permeability of SC CO₂ through several mesoporous membranes / **Problems in the flow determination using microporous membranes (small values, non-reported)**

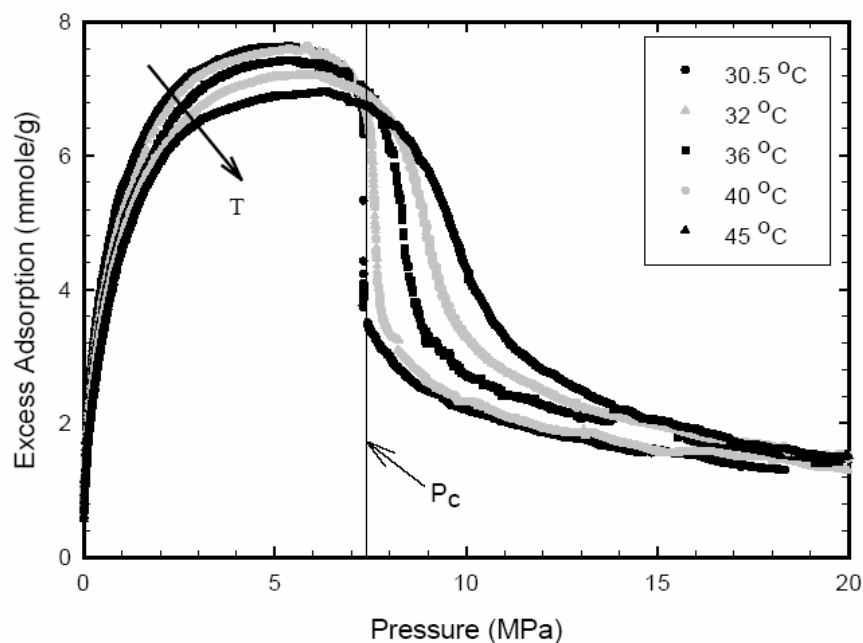
Romero et al., 2004: Unified approach for liquid, gas and SC mass transfer through microporous membranes / **Adsorption effect taking into account a Langmuir isotherm**



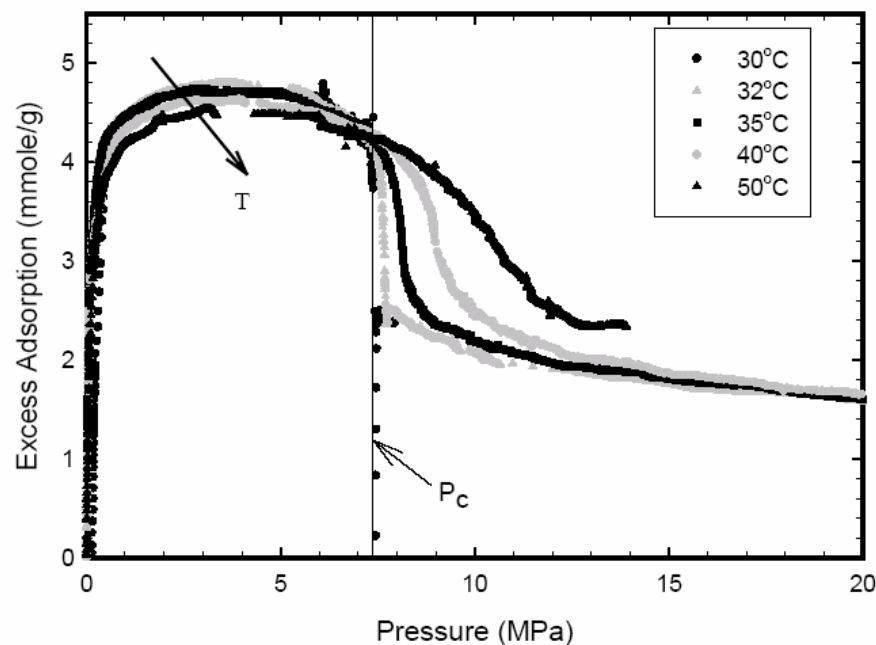
how is the adsorption within micropores at high pressure conditions?



High pressure adsorption isotherms in microporous materials



(a)



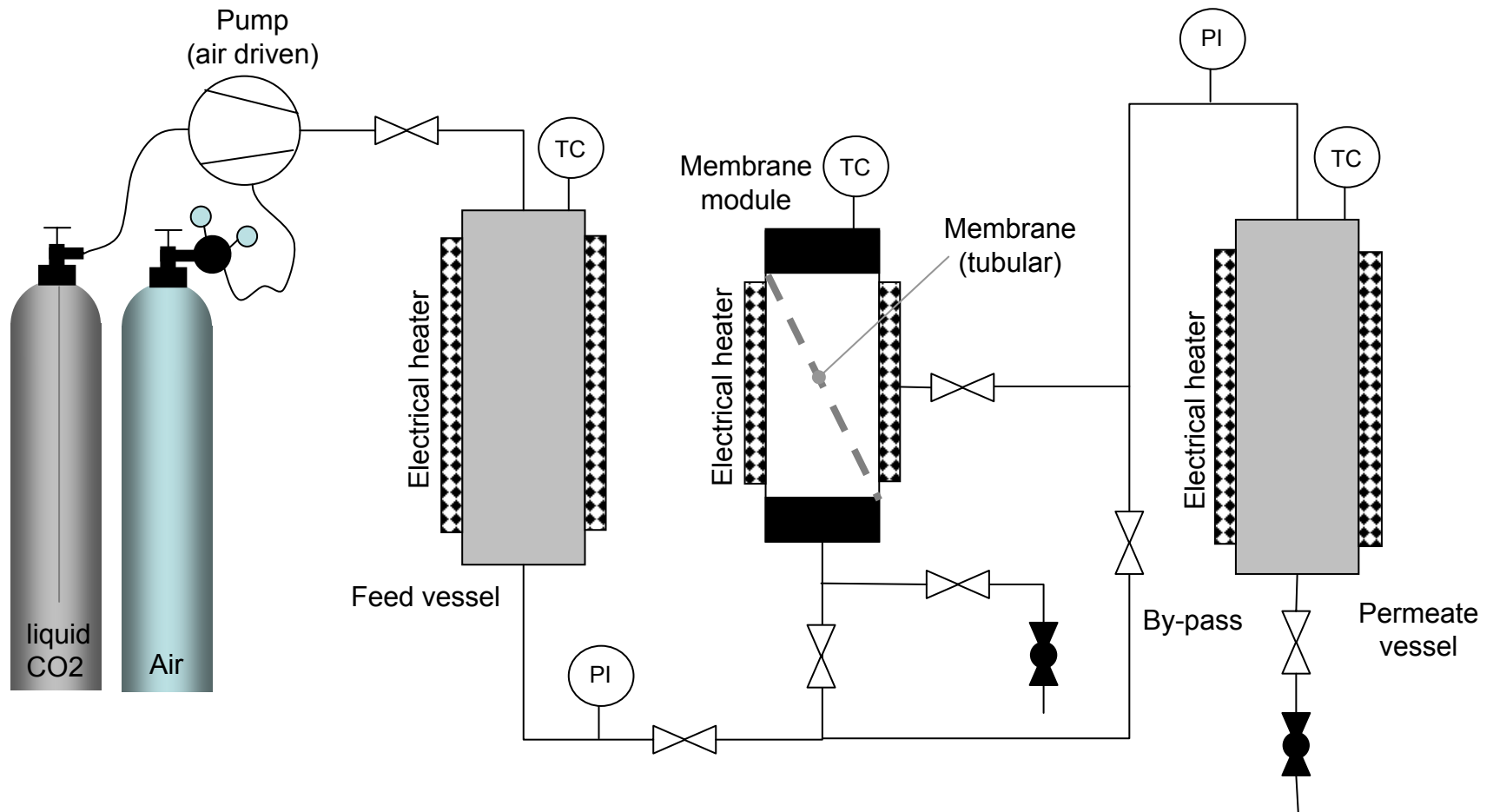
(b)

Figure 2. Adsorption of CO₂ on GAC (a) and NaY zeolite (b) showing the crossover behavior

S1: PERMEATION OF SCF THROUGH MICROPOROUS MEMBRANES



Simplified flow sheet: equipment for SCF permeability through membranes by transient method



S1: PERMEATION OF SCF THROUGH MICROPOROUS MEMBRANES



Equipment for permeability determination of gases and supercritical fluids

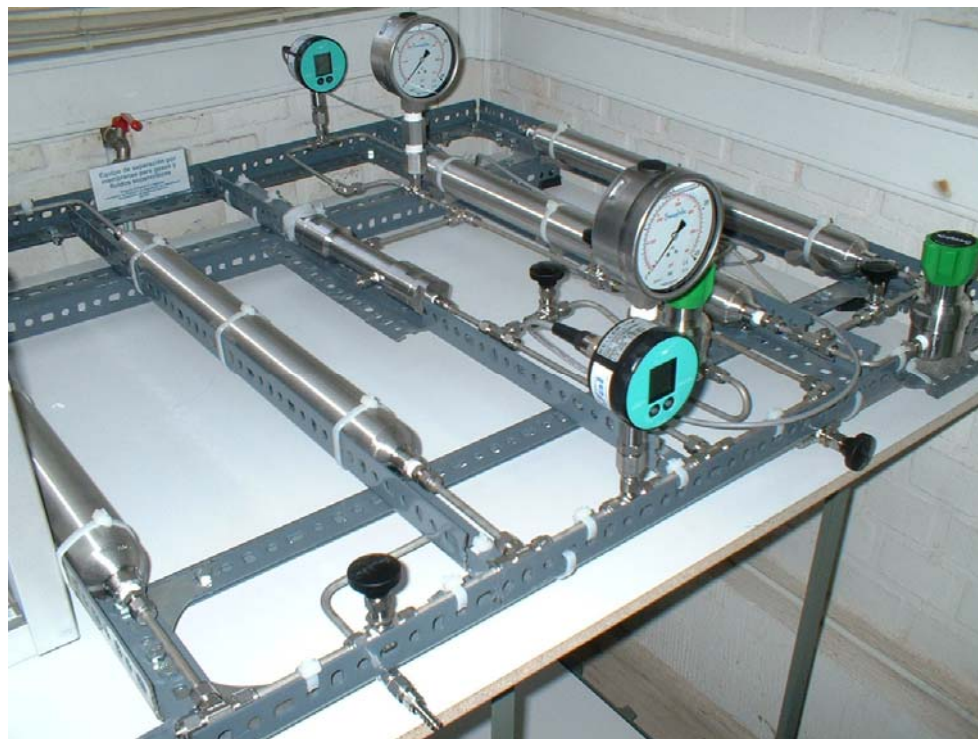
Project FONDECYT 1040240

Compression unit:

- Liquid CO₂ pump (5 L/h, 250 bar)
- Air driven

Permeation unit:

- Pressure (700 bar)
- Temperature (25-250°C)
- Feed and permeate vessels (0.5-1.0 L)
- Inorganic membrane module
- zeolite membrane (L = 15 cm, D = 1 cm)



S1: PERMEATION OF SCF THROUGH MICROPOROUS MEMBRANES



Modeling SC CO₂ permeation through MFI zeolite membrane

(Navarrete and Romero, 2004)

Mechanism proposed: Surface diffusion *(Krishna, 1993)*

Mass transfer model proposed: Darken equation *(Burggraaf and Cot, 1996)*

$$J_i = -\varphi \cdot D_{0,i} \cdot \frac{\delta \ln(P)}{\delta \ln(q_i)} \cdot \frac{dq_i}{dz}$$

$$\int J_i \cdot dz = - \int_{q_{f,i}}^{q_{p,i}} \varphi \cdot D_{0,i}(q_i) \cdot \Gamma \cdot dq$$

Γ = Thermodynamic factor

Modeling carrying out numerical resolution of the integral with the Thermodynamic Factor using adsorption experimental data

S1: CONCLUSIONS AND CHALLENGES



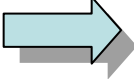
SCF/Inorganic membranes: possibility of proposing several processes and configurations (separation, membrane reactor = reaction + separation)

The microporous membrane gives a particular thermodynamic condition of the fluid within the pore (liquid = gas = SCF)

Can different mechanisms be observed (sorption, diffusion, etc....)?

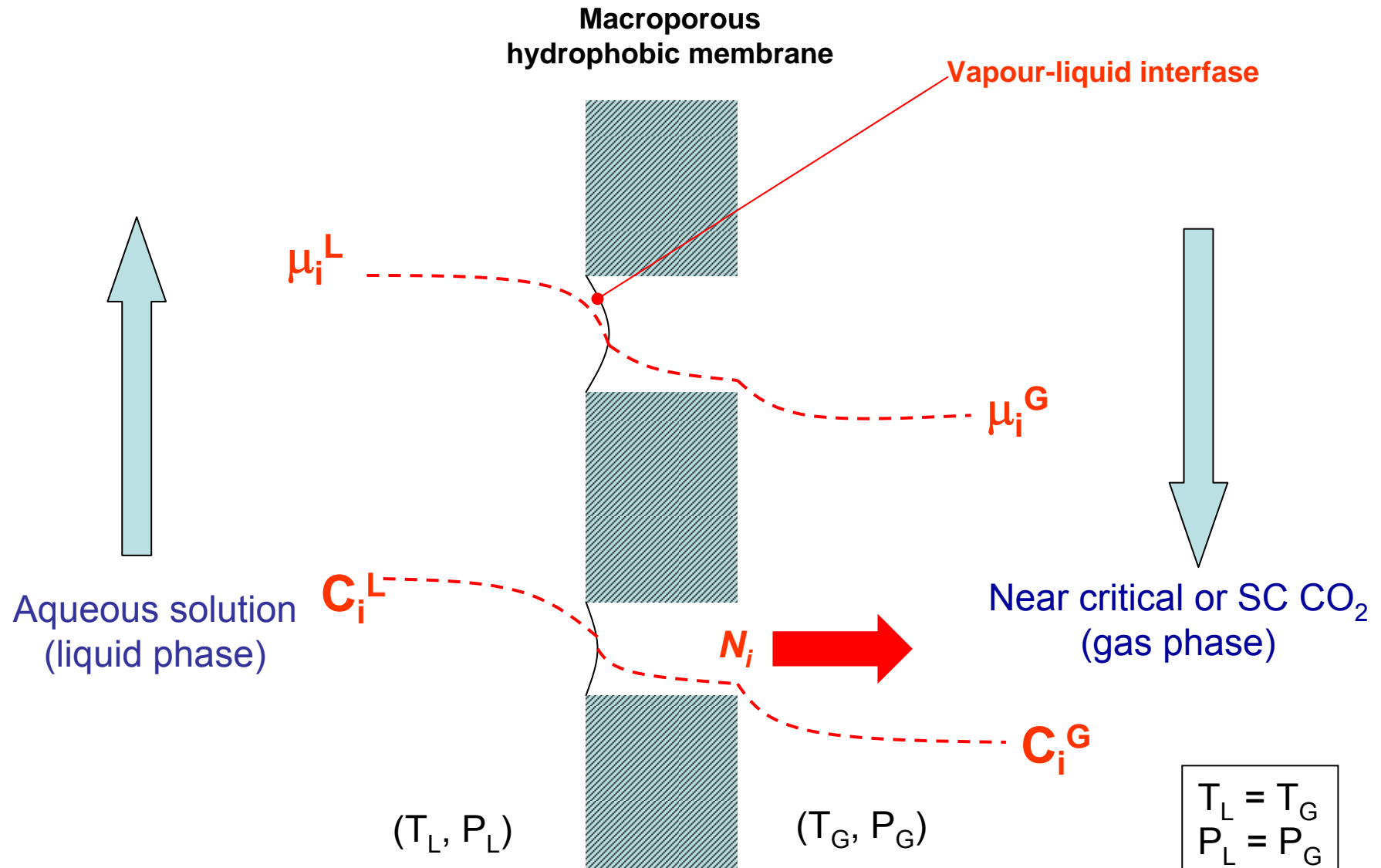
Adsorption effects observed: new model incorporates these aspects for SCF



 **Subject 1:** Permeability and selectivity determination of SCF through microporous membranes

Subject 2: Modeling of the extraction by membrane contactors using supercritical solvents: simulations of porocritical extraction

S2: MEMBRANE CONTACTORS USING SC SOLVENTS





Why to carry out SFE using a membrane contactor?

- Porocritical fluid extraction is a efficient alternative to conventional contacting columns which disperse one fluid phase in another
- Advantages include high throughput capacity without column flooding or emulsion formation, independence of density between solvent and feed, and modularity of design (There are no large expensive vessels in a typical PoroCrit application, just pipes and pumps)
- The reduced process complexity and expense can enable a broader industrial use of carbon dioxide's attributes as a non-toxic, environmentally benign extraction solvent.
- A hollow fiber membrane contactor is usually 100 times more efficient on a volumetric basis (m^2/m^3) than a conventional contactor.

S2: MEMBRANE CONTACTORS USING SC SOLVENTS



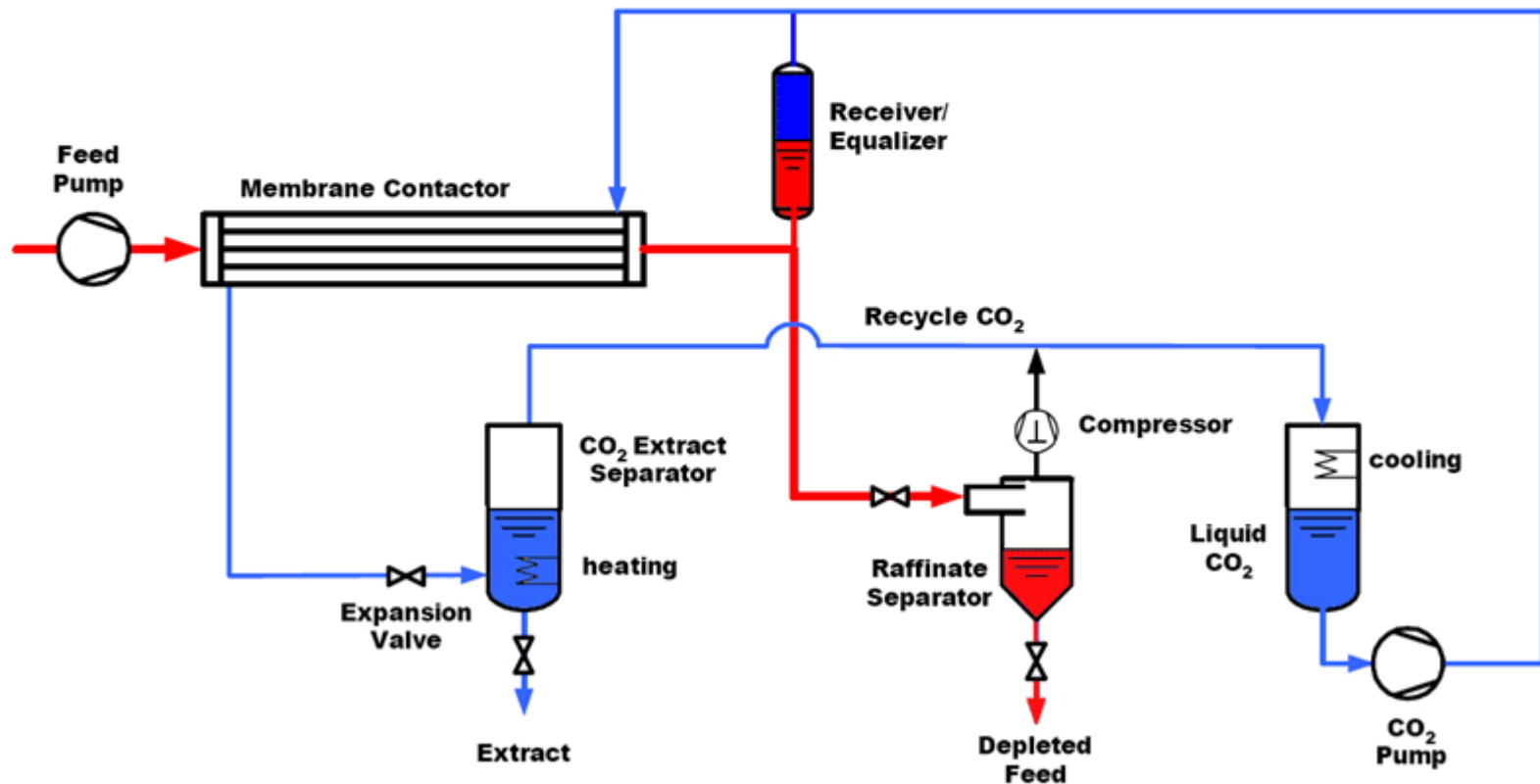
Comparison of Contactors in Solvent Extraction

CHARACTERISTIC	CONVENTIONAL	MEMBRANE CONTACTOR
Can form emulsion	yes	no
Requires fluid density differences	yes	no
Contact area per volume (efficiency)	1	10-100
Modular design	no	yes
Limited throughput and velocity	yes	no
Maintain sterility	no	yes
Cleans without dismantling	no	yes
Handles suspensions	no	yes
Breaks emulsions	no	yes

S2: MEMBRANE CONTACTORS USING SC SOLVENTS



Commercial Scale Continuous Countercurrent Porocritical Fluid Extraction/Purification





Modeling PoroCrit® extraction

Model based on a system constituted by three mass transfer resistances in series:

- 1) Liquid boundary layer
- 2) Stagnant gas layer within the membrane porosity (and VLE)
- 3) Gas boundary layer

$$\frac{1}{K_W} = \frac{1}{k_W} + \frac{d_i}{d_{ML} k_m m_i} + \frac{d_i}{d_o k_o m_i}$$

$$\Delta C_{ML} = \frac{(C_l - C_{sc} / m_i)_1 - (C_l - C_{sc} / m_i)_2}{\ln \left[\frac{(C_l - C_{sc} / m_i)_1}{(C_l - C_{sc} / m_i)_2} \right]}$$

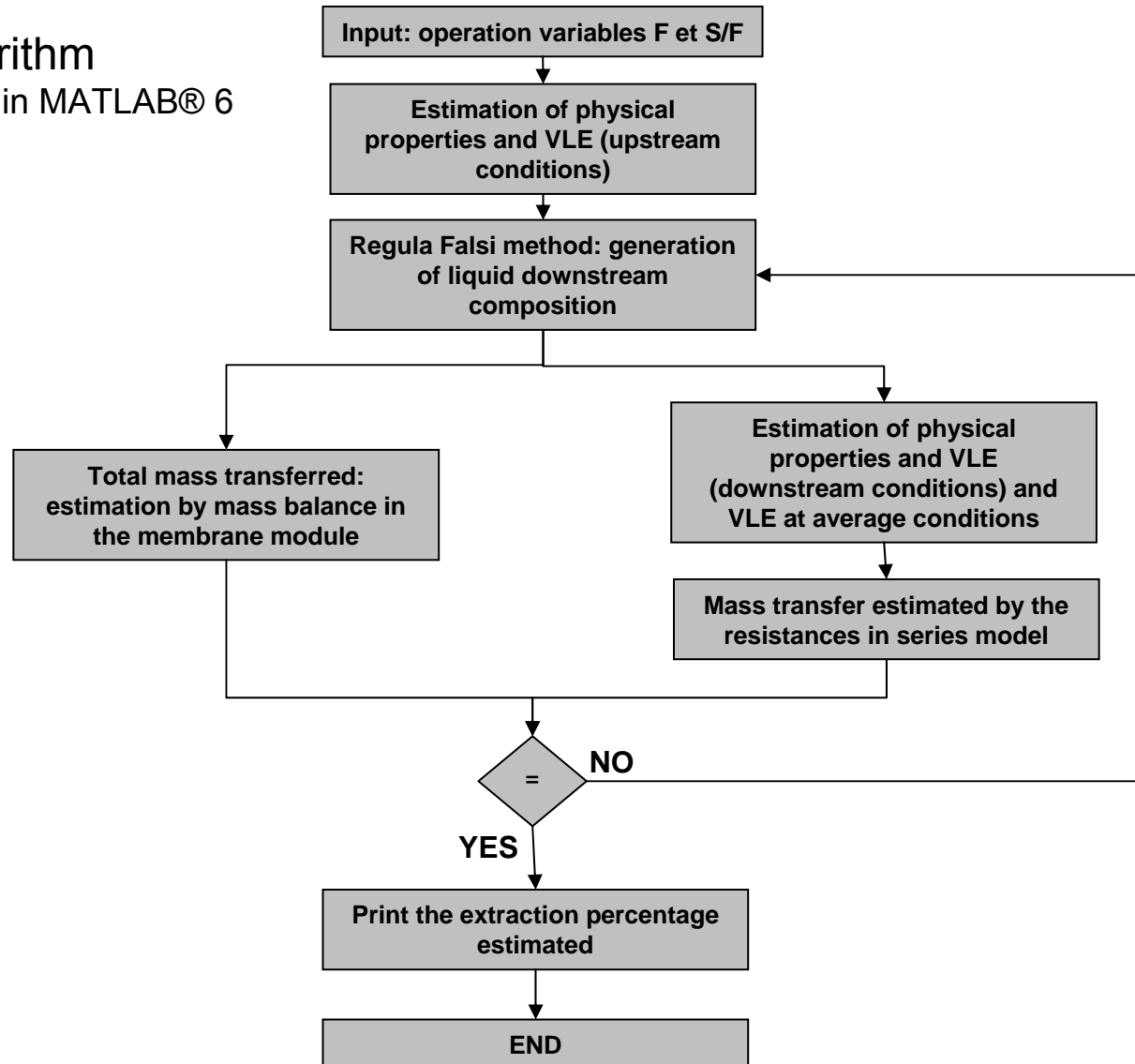
$$m_i = \frac{C_{sc}}{C_l} : \text{Partition coefficient}$$

S2: MEMBRANE CONTACTORS USING SC SOLVENTS



Simulation algorithm

Program developed in MATLAB® 6



S2: MEMBRANE CONTACTORS USING SC SOLVENTS



Equations for prediction of properties in liquid phase (water-ethanol)

Property	System	Equation	Authors
Density	water-ethanol	$\rho = a \exp \left[-\frac{(X-b)^2}{2c^2} \right]$	Perry et al., 2000 Estay and Romero, 2004
Viscosity	water -ethanol		Estay and Romero, 2004
Diffusion coefficient	water -ethanol		Reid et al., 1977 Perry et al., 2000

S2: MEMBRANE CONTACTORS USING SC SOLVENTS



Equations for prediction of properties in gas phase (CO₂-ethanol)

Property	System	Equation	Authors
Density	CO ₂ -ethanol	PR EOS	Brunner, 1994
Viscosity	CO ₂ -ethanol	Chung et al	Chung et al., 1988
Diffusion coefficient	CO ₂ -ethanol	Catchpole et al	Catchpole and King, 1994

S2: MEMBRANE CONTACTORS USING SC SOLVENTS



Conditions used for the simulations

Operation conditions of experiments (Bothum et al., 2003)

Pressure (liquid and gas)	69 bar
Temperature	298 K
Composition of liquid feed (X_{EtOH} , X_{acetone})	10 % w/w

Structural parameters of the membrane contactor

Membrane material	Polypropylene
Number of fibers, n	1
Length, L	1.07 m
Internal diameter, d_{in}	0.6 mm
External diameter, d_{out}	1.02 mm
Pore diameter, d_p	0.2 μm
Porosity, ε	75 %

S2: MEMBRANE CONTACTORS USING SC SOLVENTS



Extraction percentage (**EX**) of **ethanol** from the aqueous solution through porocritical extraction in function of the liquid flow (**F**) and the molar flow ratio sweep gas/liquid (**S/F**)

F (mL/min)	S/F	EX_{EXP} (%)	EX_{EST} (%)
0.15	3	15.2 ± 0.5	16.17
0.25	3	10.4 ± 0.5	13.31
0.5	3	4.7 ± 1.8	13.61
1.0	3	9.9 ± 0.5	9.67
0.1	10	31.9 ± 1.4	34.00

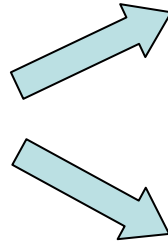
Extraction percentage (**EX**) of **acetone** from the aqueous solution through porocritical extraction in function of the liquid flow (**F**) and the molar flow ratio sweep gas/liquid (**S/F**)

F (mL/min)	S/F	EX_{EXP} (%)	EX_{EST} (%)
0.15	3	96.1 ± 1.8	95.04
0.25	3	89.6 ± 1.8	88.31
0.5	3	68.9 ± 1.8	75.56
1.0	3	67.9 ± 1.8	58.12

S2: CONCLUSIONS AND CHALLENGES



Coupled processes = coupled effects



Vapour-liquid equilibrium (VLE)



Mass transfer resistances in series
(gas and liquid boundary layers and membrane pores)

Stability of the interfaces: good control of operation variables and easy scale-up

Potential applications:

- | | |
|-------------------|-------------------------|
| ✓ Foods | ✓ Pollution remediation |
| ✓ Biotechnology | ✓ Chemical analysis |
| ✓ Chemicals | ✓ Polymers |
| ✓ Cosmetics | ✓ Pasteurización |
| ✓ Pharmaceuticals | ✓ Solvent recovery |



**Monofiber membrane
module for porocritical
extraction (LPSM, USACH)**

GENERAL CONCLUSIONS



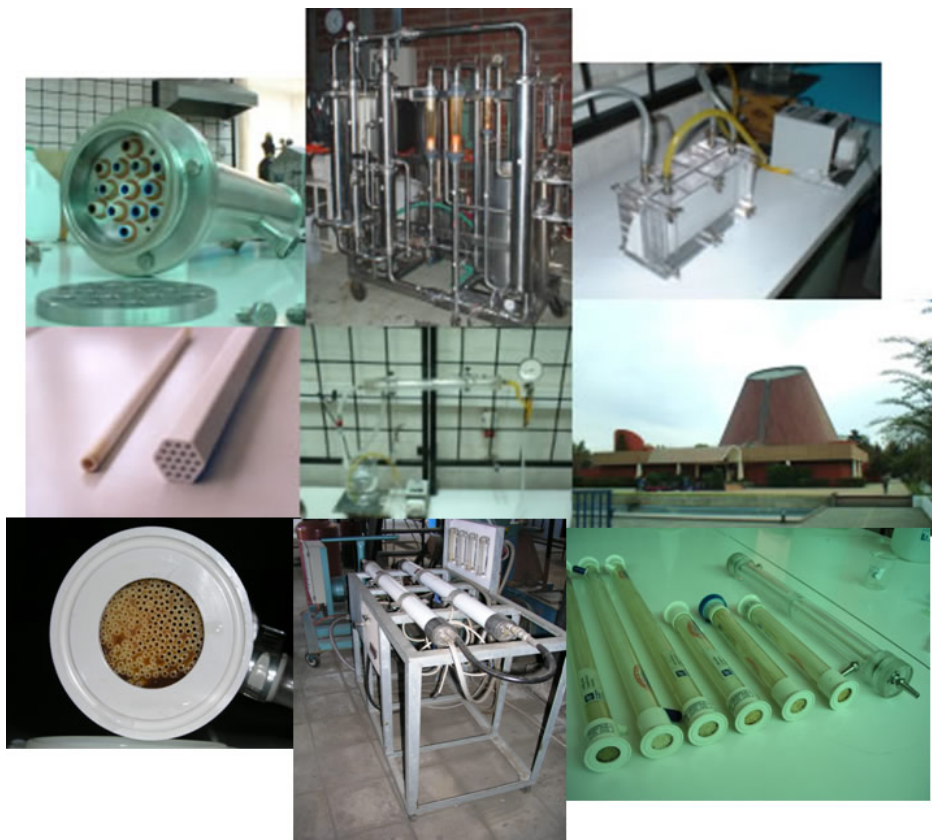
The use of a membrane in presence of a supercritical fluid makes possible the design of very attractive and powerful processes

Several processes and configurations: improve transfer or reaction, to set in contact phases, to fluidify highly viscous liquids

Overall the major interest of all the processes thus created is to be safeguarding for environment and products, which is in particular essential when these ones are of biological nature

The principal effort requested from the researcher is a whole effort of imagination, and serious in further investigation with appropriate knowledge of membranes and supercritical fluid technologies

Thank you for your attention



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